



Simulation study of L/H transition with self-consistent integrated modelling of core and SOL/Divertor transport

**M. Yagi^{1,2}, K. Shimizu³, T. Takizuka³, M. Honda³,
N. Hayashi³, K. Hoshino² and A. Fukuyama⁴**

¹ Research Institute for Applied Mechanics, Kyushu University

² Japan Atomic Energy Agency, Rokkasho

³ Japan Atomic Energy Agency, Naka

⁴ Graduate School of Engineering, Kyoto University

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Contents of My Talk

■Activity of Integrated Transport Modelling in Japan

BPSI, (BA IFERC/CSC)

■Core-Edge Coupling Model: TASK/TOPICS + SONIC

■Application of TOPICS+SONIC to L/H Transition Dynamics

- Empirical Transport Model**

K. Shimizu et al., 23th FEC, Daejon, 2010, THD/5-2Ra

- Tuned Current Diffusive Ballooning Model (CDBM) Transport Model**

First Topic

✓Activity of Integrated Transport Modelling in Japan

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■Application of TOPICS+SONIC to L/H Transition Dynamics

- Empirical Transport Model**

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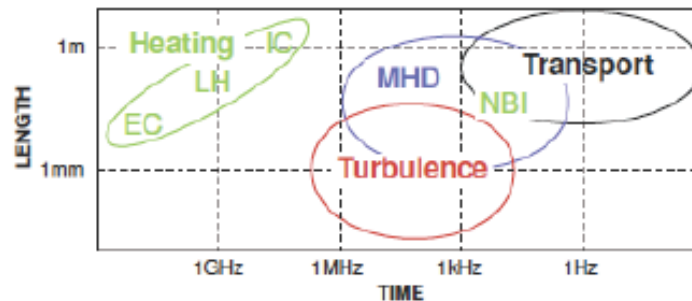
- Tuned Current Diffusive Ballooning Model (CDBM) Transport Model**

GENERAL OUTLINE

Establishment of quantitative description of burning plasmas in ITER

Development of integrated transport simulation
with various modules

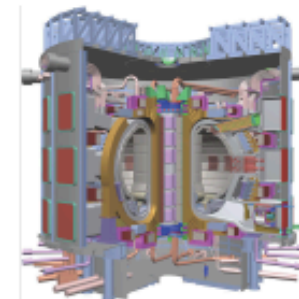
A. Fukuyama and M. Yagi, 'Burning Plasma Simulation Initiative and Its Recent Progress', J. Plasma Fusion Res. Vol.81, No.10 (2005) 747-754.



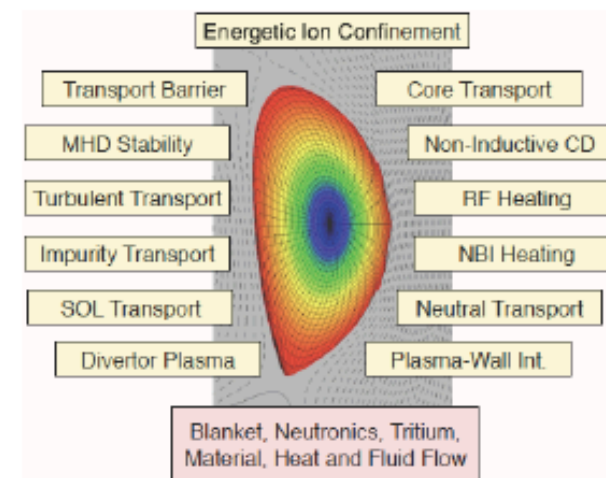
Time scale 10ps (100GHz)~1000s, spatial scale 10 μ m~10m

Burning plasma includes multi-scale, multi-physics phenomena

ITER

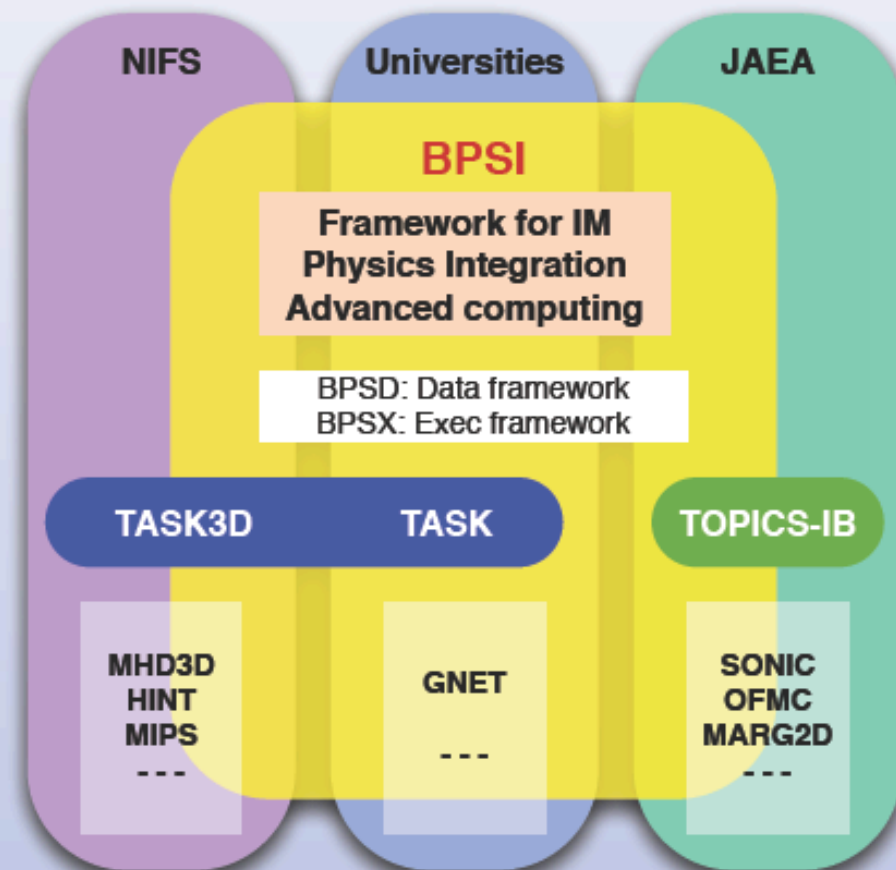


Reliable prediction
and control



Integrated Modeling Activity in Japan

Burning Plasma Simulation Initiative (BPSI)
Research collaboration of universities, NIFS and JAEA



BA Site in Rokkasho

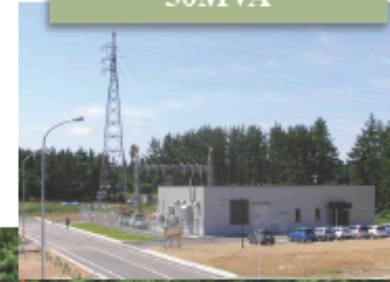
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- In March, 2010 main buildings in BA site are completed.

IFMIF/EVEDA Accelerator Bld.



Power Station
30MVA



守衛所



DEMO R&D Bld.



Computer Simulation &
Remote Experimentation
Bld.



Administration & Research Bld.



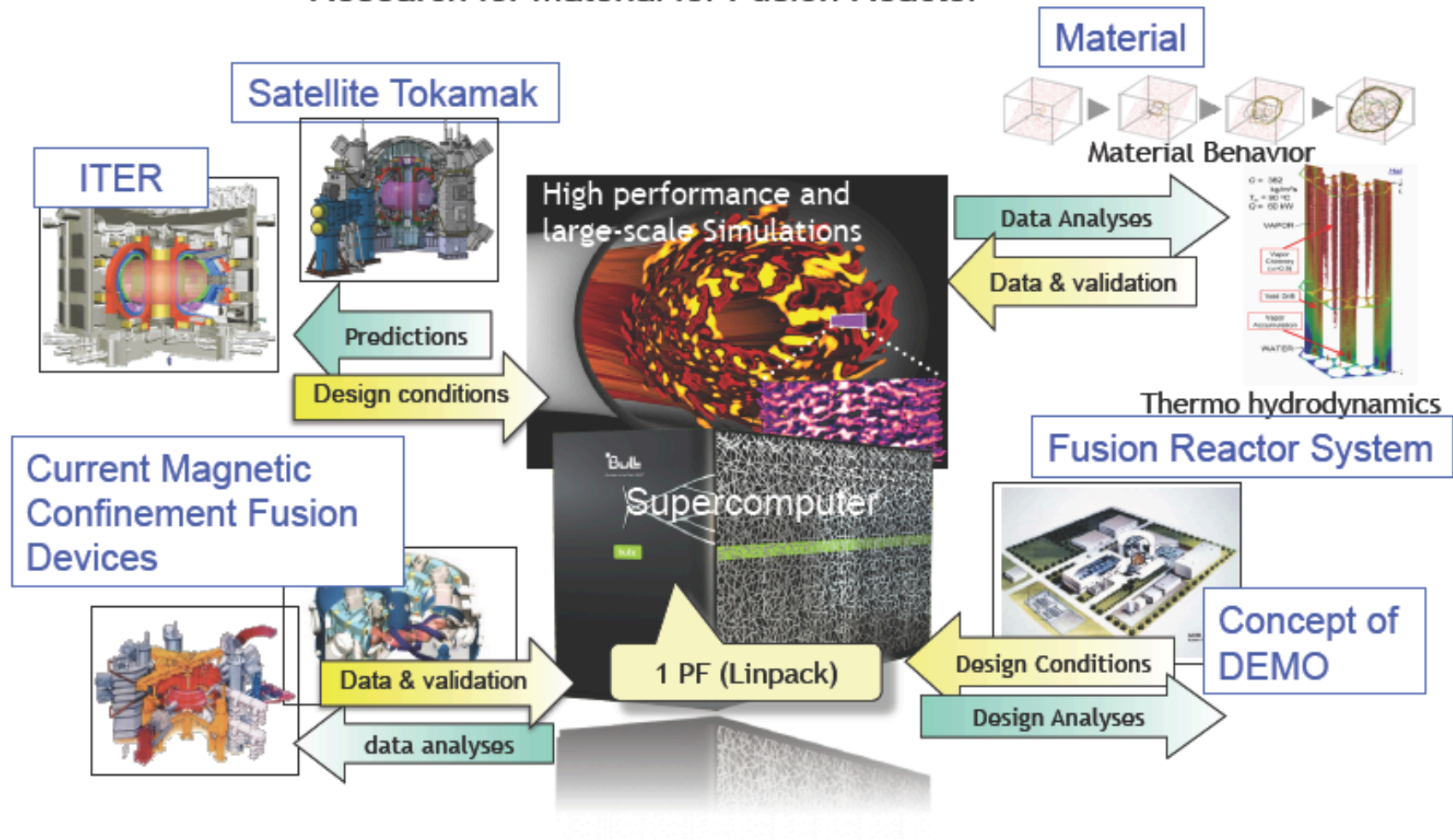
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Research Fields for IFERC CSC High Performance Computing System



- Plasma Physics for the Magnetic Confinement Fusion
- Research for Fusion Development (ITER & BA)
- Research for DEMO Design and R&D
- Research for Material for Fusion Reactor



Second Topic

■Activity of Integrated Transport Modelling in Japan

BPSI, (BA IFERC/CSC)

✓Core-Edge Coupling Model: TASK/TOPICS + SONIC

■Application of TOPICS+SONIC to L/H Transition Dynamics

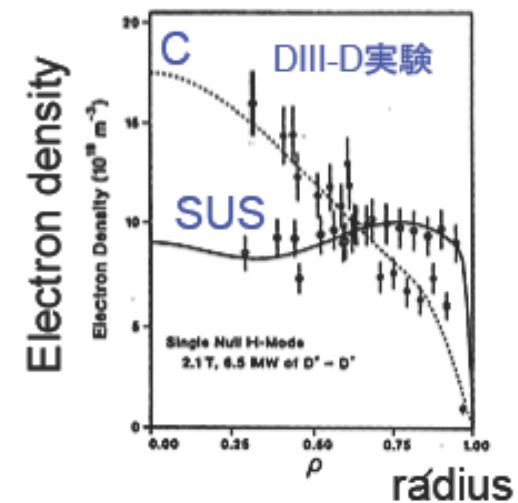
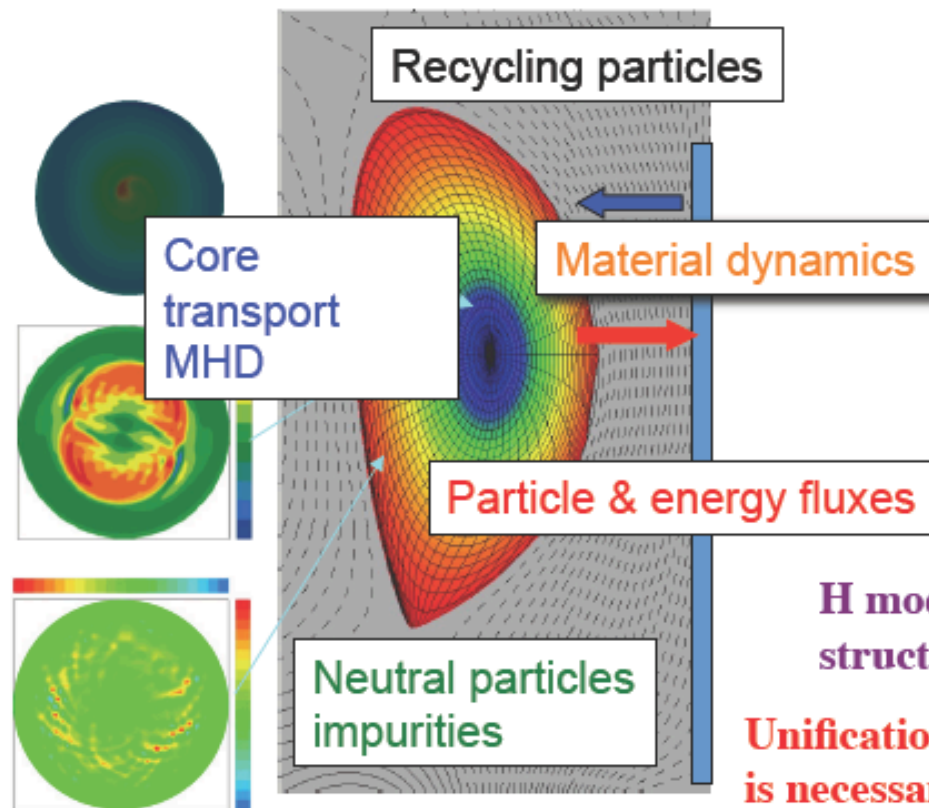
- Empirical Transport Model**

K. Shimizu et al., 23th FEC, Daejon, 2010, THD/5-2Ra

- Tuned Current Diffusive Ballooning Model (CDBM) Transport Model**

Integrated Transport Code

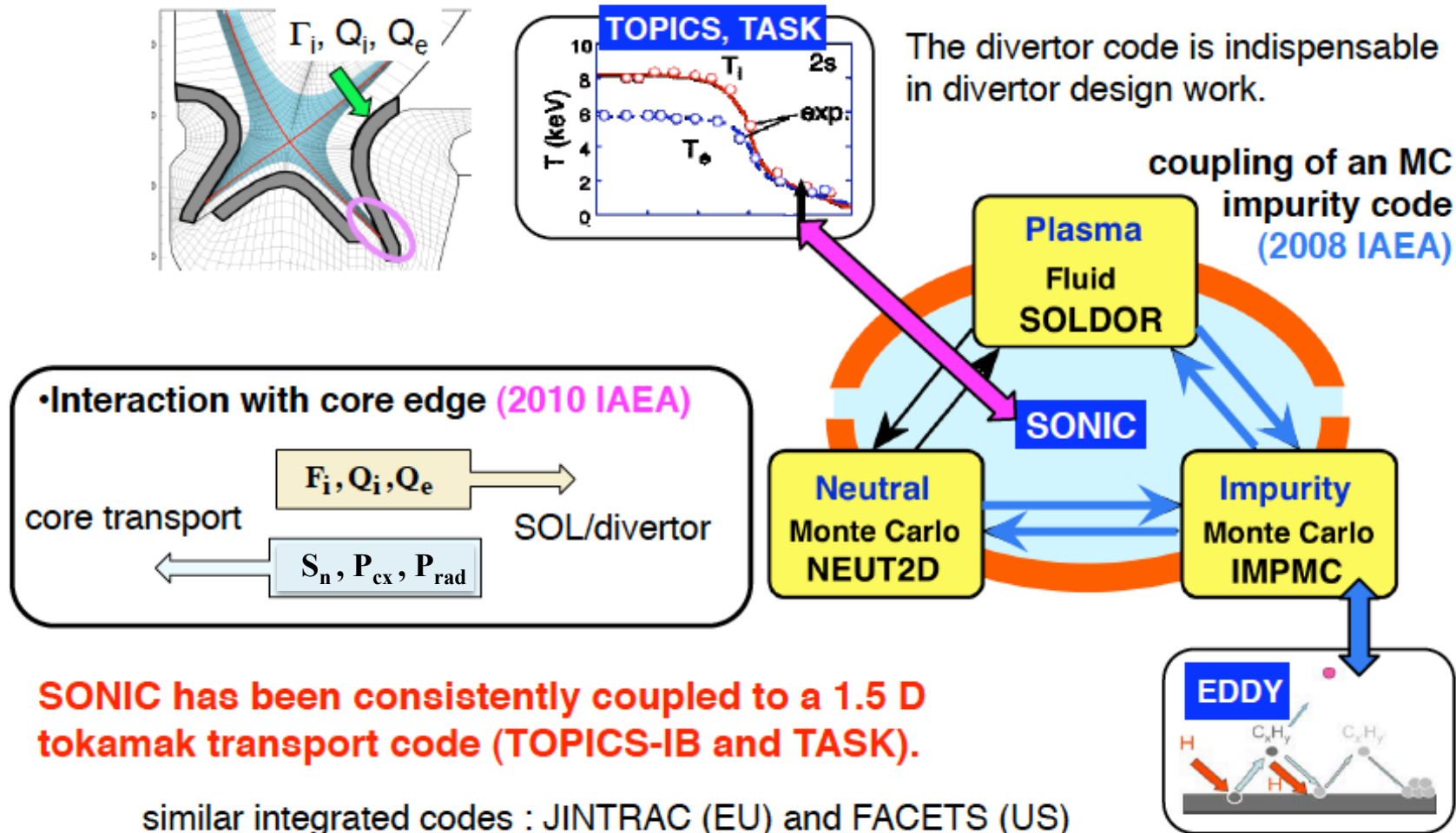
Inclusion of plasma, atomic/molecule and material dynamics
Handle with multi-scale, multi-physics, complex phenomena



H mode characteristics depends on structural material

Unification of plasma science and material science is necessary for the success of ITER

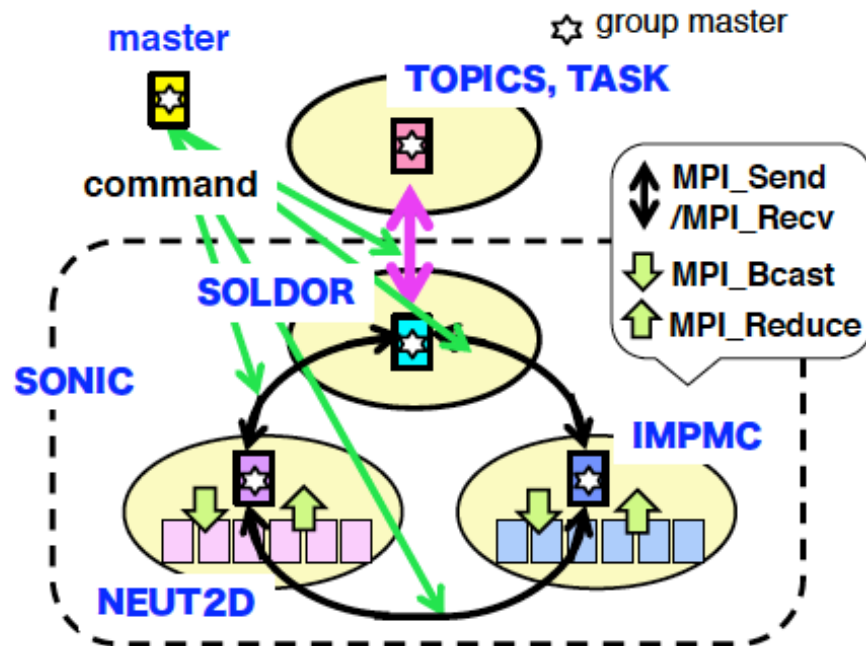
Integrated Divertor Code “SONIC”



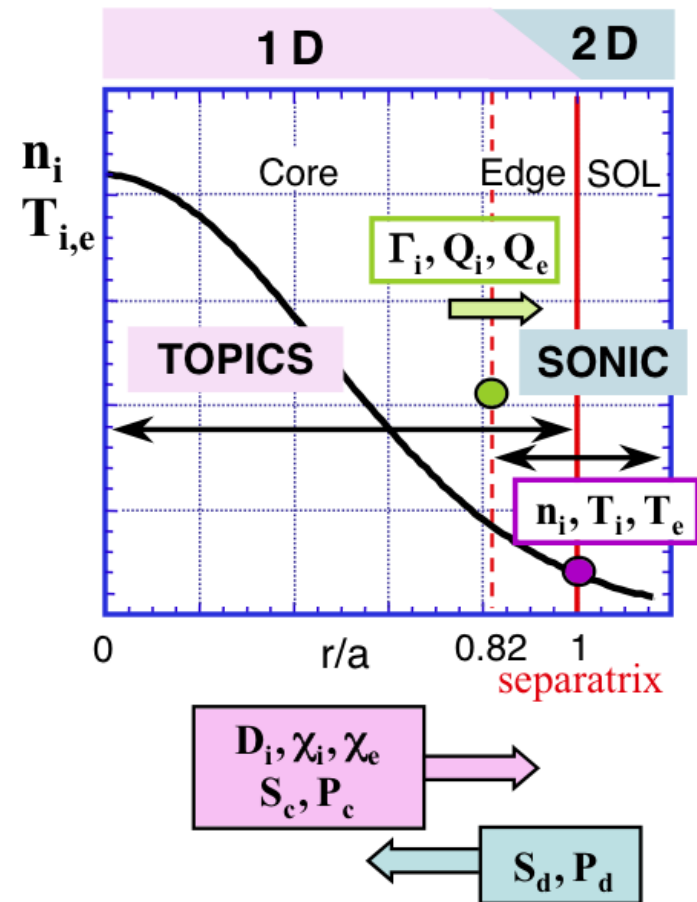
Coupling to the Core Transport Code

New MPMD parallel computing System

enables unification of independently established code suite efficiently.



Relation between TOPICS and SONIC



Data exchange in every 200 μ s

Third Topic

■Activity of Integrated Transport Modelling in Japan

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✓Application of TOPICS+SONIC to L/H Transition Dynamics

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Transport Modelling

High current operation of JT-60SA ($I_p = 5.5$ MA, $B_T = 2.25$ T)

Diffusion coef. in the main plasma

(simple empirical model : Hayashi N. et al. 2009
Nucl. Fusion **49** 095015)

$$\chi_i(\rho) = \chi_e(\rho) = 2 \times D_i(\rho) \\ = 0.3 \cdot (1 + 2\rho^2) \times \sqrt{1 + P_{NB}/P_{OH}} \text{ m}^2/\text{s}$$

H-mode phase $0.9 < r/a < 1.0$

$$D_i = 0.1 \text{ m}^2/\text{s}, \chi_i = \chi_e = 0.2 \text{ m}^2/\text{s}$$

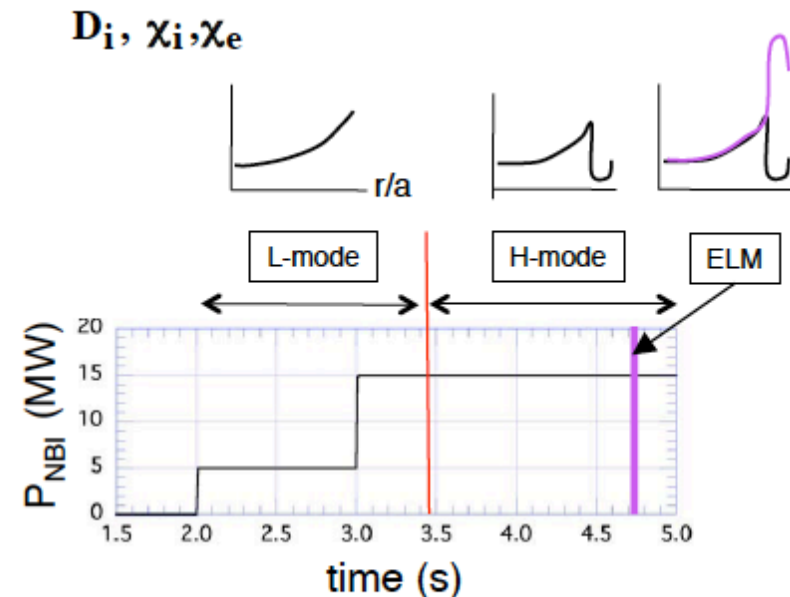
Diffusion enhanced by ELM crash

$$D_i = 50 \text{ m}^2/\text{s}, \chi_i = \chi_e = 50 \text{ m}^2/\text{s} \\ \text{during } 200 \mu\text{s}$$

Diffusion coef. in SOL/Divertor region

are fixed throughout the simulation;

$$D_i = 0.3 \text{ m}^2/\text{s}, \chi_i = \chi_e = 1 \text{ m}^2/\text{s}$$



For simplicity (mainly to reduce cpu time),
simple radiation model (Non coronal model)
is employed instead of IMPMC.

Evolution of profiles after the L-H transition

Radial profile **in the core**

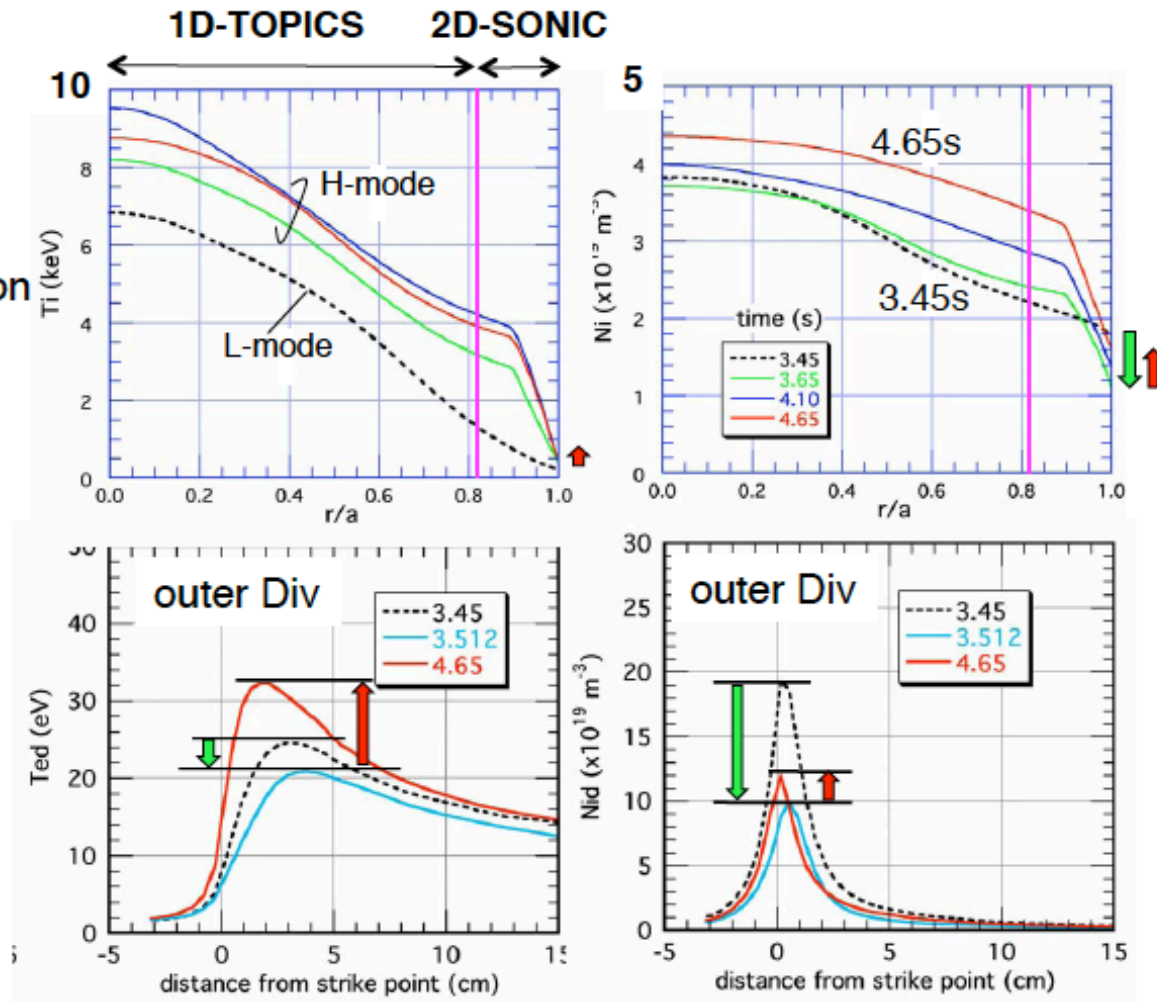
Pedestal Ni and Ti grow up in the H-mode

Separatrix Ni is reduced by reduction in Fi at the transition and gradually increases with the recovery of Fi.

Profile **along divertor plate**

Peak values of Nid and Ted are reduced by small Fi and Qe after the transition.

Afterwards Nid and Ted gradually increase.



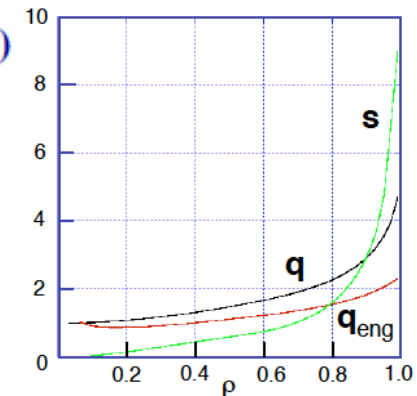
Tuned CDBM Model

$$\chi_{\text{CDBM}} = \frac{c^2}{\omega_{\text{pe}}^2} \frac{v_A}{qR} |\alpha|^{3/2} F(s, \alpha), \quad \alpha = -q^2 R \frac{d\beta}{dr} \quad (\text{K. Itoh et al., PPCF, 1994})$$

■ At the edge, $\chi \approx \frac{q^3(1)}{s^{1/2}}$ can not decrease due to large $q(1)$

✓ **Modification (I)** Using Engineering q

$$q(r) \equiv q_{\text{eng}}(r) = \frac{2\pi k r^2 B_t}{\mu_0 R I(r)}$$

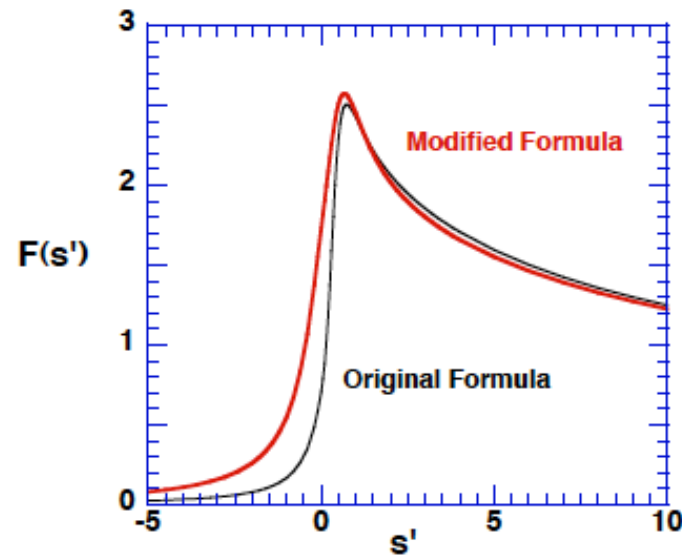


■ In the weak-shear central region, F is very small and the ITB can be easily formed by the heating power smaller than an ETB threshold (L-H transition).

✓ **Modification (II)** Moderate decrease of F for $s' < 0$ regime

$$F(s, \alpha) \equiv F(s') = \begin{cases} \sqrt{3}(1 + 2s'^{2.5}) / (1 - s' + 1.35s'^2 + 0.7698s'^3), & s' > 0 \\ \sqrt{3} / [(1 - s')(1 - s' + 3s'^2)]^{1/2}, & s' < 0 \end{cases} \quad s' \equiv s - \alpha$$

Tuned CDBM Model (Cont.)



■ In the weak-shear central region, $(\omega_{\text{EXB}}/\gamma_{\text{CDBM}})$ becomes very small and the ITB can be easily formed before the L-H transition.

✓ **Modification (III)** Modification of shear dependence on γ_{CDBM}

$$\gamma_{\text{CDBM}} = |\alpha|^{1/2} \frac{v_A}{qR} F(s') \quad (\text{J.W. Connor, PPCF 1993})$$

Tuned CDBM Model (Cont.)

Transport Model $\chi_{\text{ANO}} = \frac{A\chi_{\text{CDBM}}}{1+(B\omega_{\text{EXB}}/\gamma_{\text{CDBM}})^K}$ **(T. S. Hahm and K.H. Burrell, PoP 1995)**

✓ Adjustment of Transport Coefficients

$$\omega_{\text{EXB}} = (RB_{\theta}/B_t) |d/dr (E_r/RB_{\theta})|$$

$$- dp_i/dr + e n_i E_r = 0$$

A: $HH \approx 0.5$ for L-mode

B: L-mode for $P_{\text{loss}} < P_{\text{LH}}$

K: $\omega_{\text{EXB}} \sim |\alpha|$, $\gamma_{\text{CDBM}} \sim |\alpha|^{1/2}$, $\chi_{\text{CDBM}} \sim |\alpha|^{3/2}$

$$\chi_{\text{ANO}} \sim \frac{|\alpha|^{3/2}}{1+C|\alpha|^{K/2}} \quad K \rightarrow 3 \quad (\text{Note that } K=4 \text{ is numerically difficult})$$

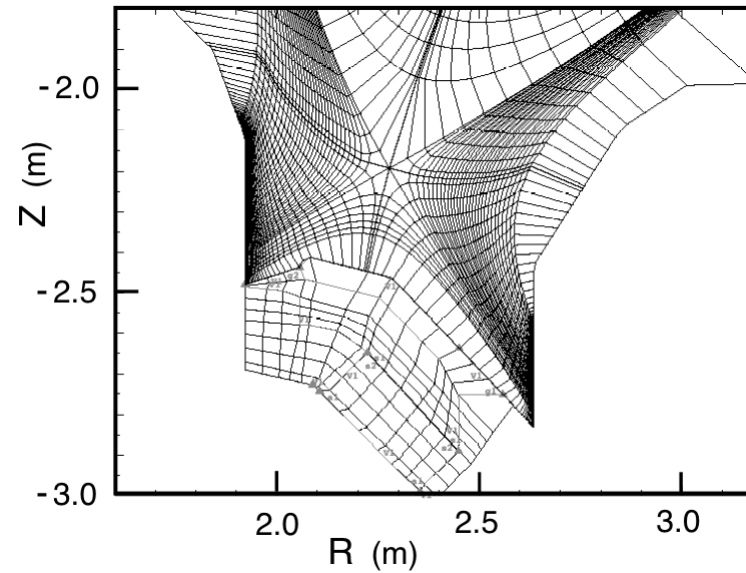
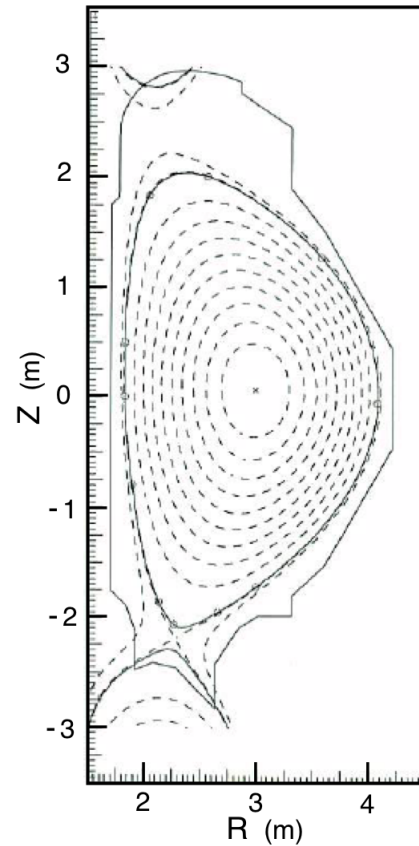
$$P_{\text{LH}} = 0.06(B_t n_{20})^{0.7} S^{0.9} \text{ (MW, T, } 10^{20} \text{m}^{-3}, \text{m}^2) \quad (\text{T. Takizuka, PPCF 2004})$$

For JT60-SA with

$$B_t = 2.3\text{T}, n_{20} = 0.3 \times 10^{20} \text{m}^{-3} \quad (n_{\text{GW}} = 1 \times 10^{20} \text{m}^{-3} \text{ for } I_p = 4\text{MA}, a = 1.13\text{m}), S = 190\text{m}^2$$

$$P_{\text{LH}} \rightarrow 5\text{MW}$$

MHD Equilibrium of JT60-SA



MHD equilibrium of a JT-60SA plasma with single-null divertor configuration. $R = 3$ m, $a = 1.1$ m, $\kappa = 1.8$, $\delta = 0.55$, $I_p = 4$ MA, and $B_t = 2.3$ T. 2D mesh configuration for SONIC is also shown.

Scenario of Transport Simulation

(1) Weak heating L-mode Phase

$P_{NB} = 0.5$ MW is added to a plasma with $I_p = 4$ MA and $B_t = 2.3$ T.

A slightly-broad current density profile $j(r)$ is given ($l_i = 0.7$).

Effective charge number $Z_{eff} = 2$ is set uniformly.

Ohmic heating power P_{OH} is calculated as 3.1 MW.

Radiation power from the core plasma is set $P_{rad} = 1$ MW.

Line average electron density is $\bar{n}_e \sim 0.25 \times 10^{20} \text{m}^{-3}$.

The HH factor by the IPB98(y,2) standard is calculated as ~ 0.5 .

(2) NB Phase

NB heating is suddenly increased up to $P_{NB} = 8$ MW at $t = 3$ s.

(3) L/H Transition Phase

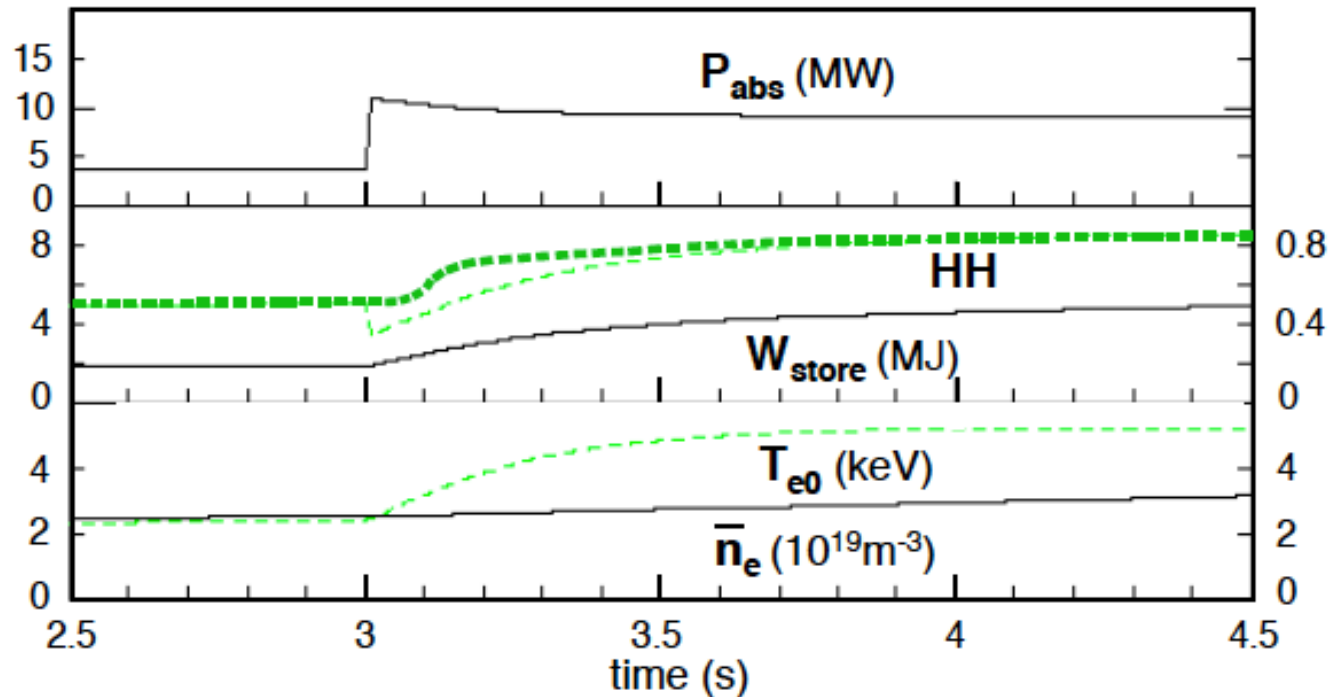
An L/H transition occurs self-consistently within the present transport model.

Absorbed power at this time, $t \approx 3.1$ s, is 10.4 MW including $P_{OH} = 2.4$ MW. Time variation of the store energy $dW/dt = 5.6$ MW.

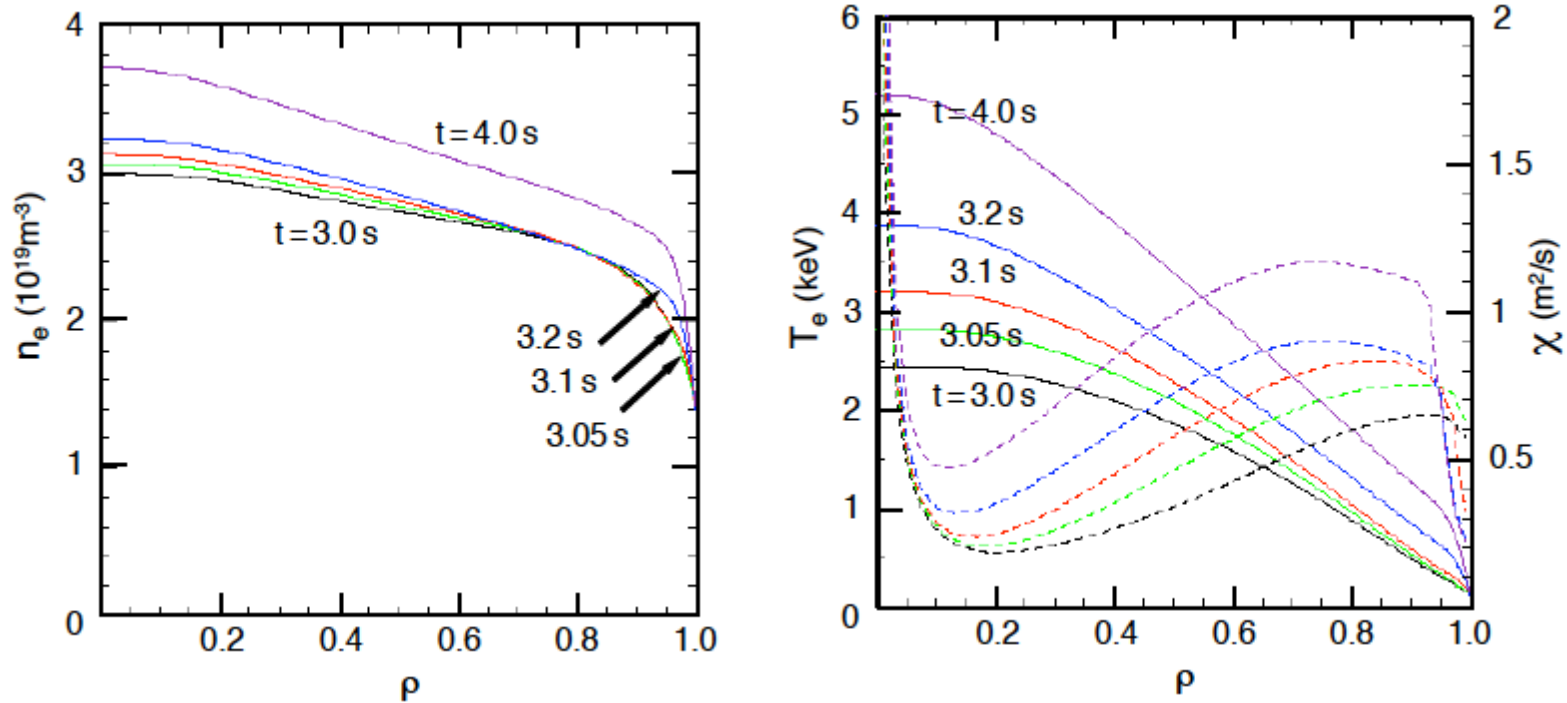
The loss power is estimated as 4.8 MW, which is similar to P_{thr} predicted by the threshold power scaling.

(4) H-mode Phase

The HH factor becomes about 0.85 in the H-mode phase.

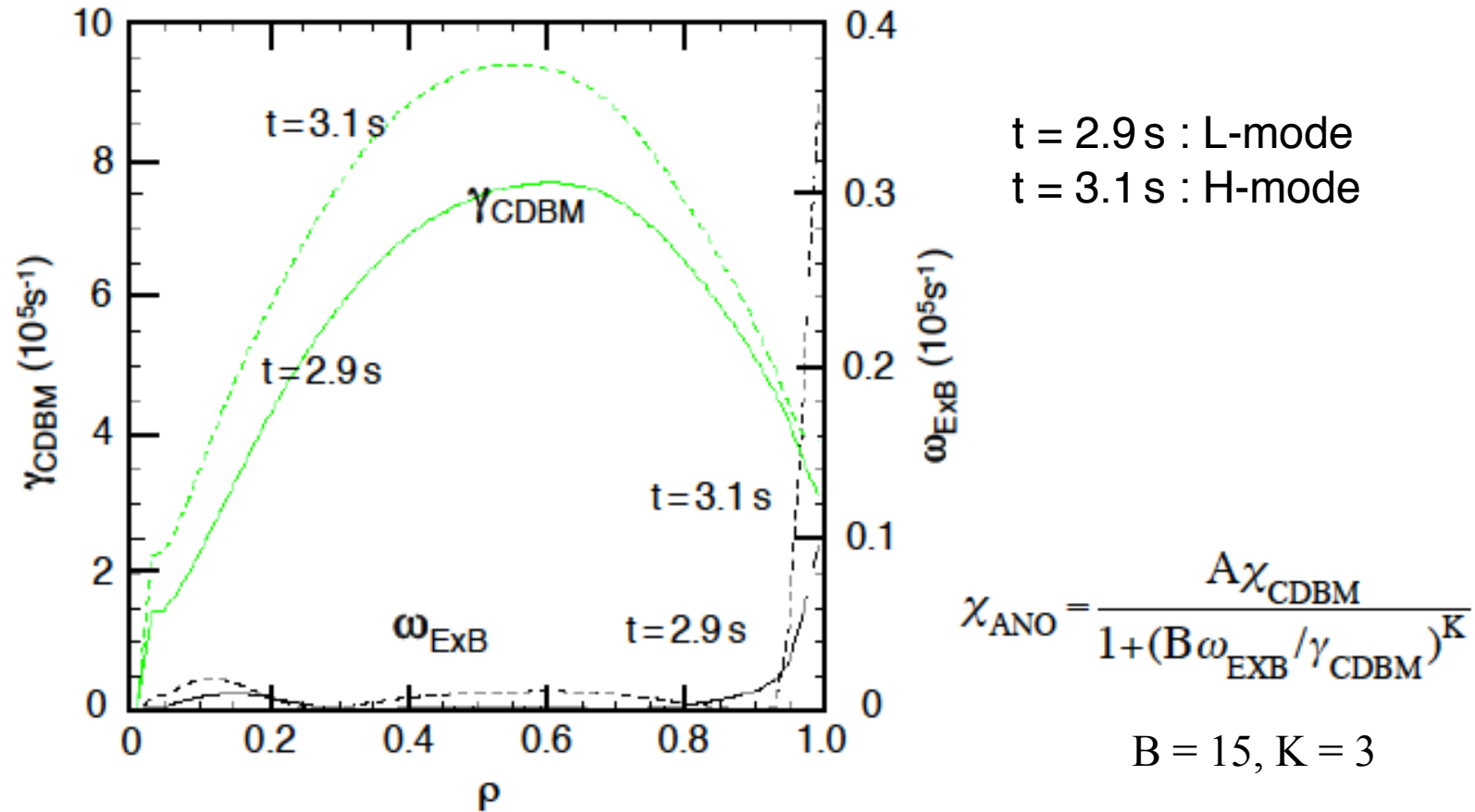


Time Evolution of Density and Temperature in L/H Transition Phase



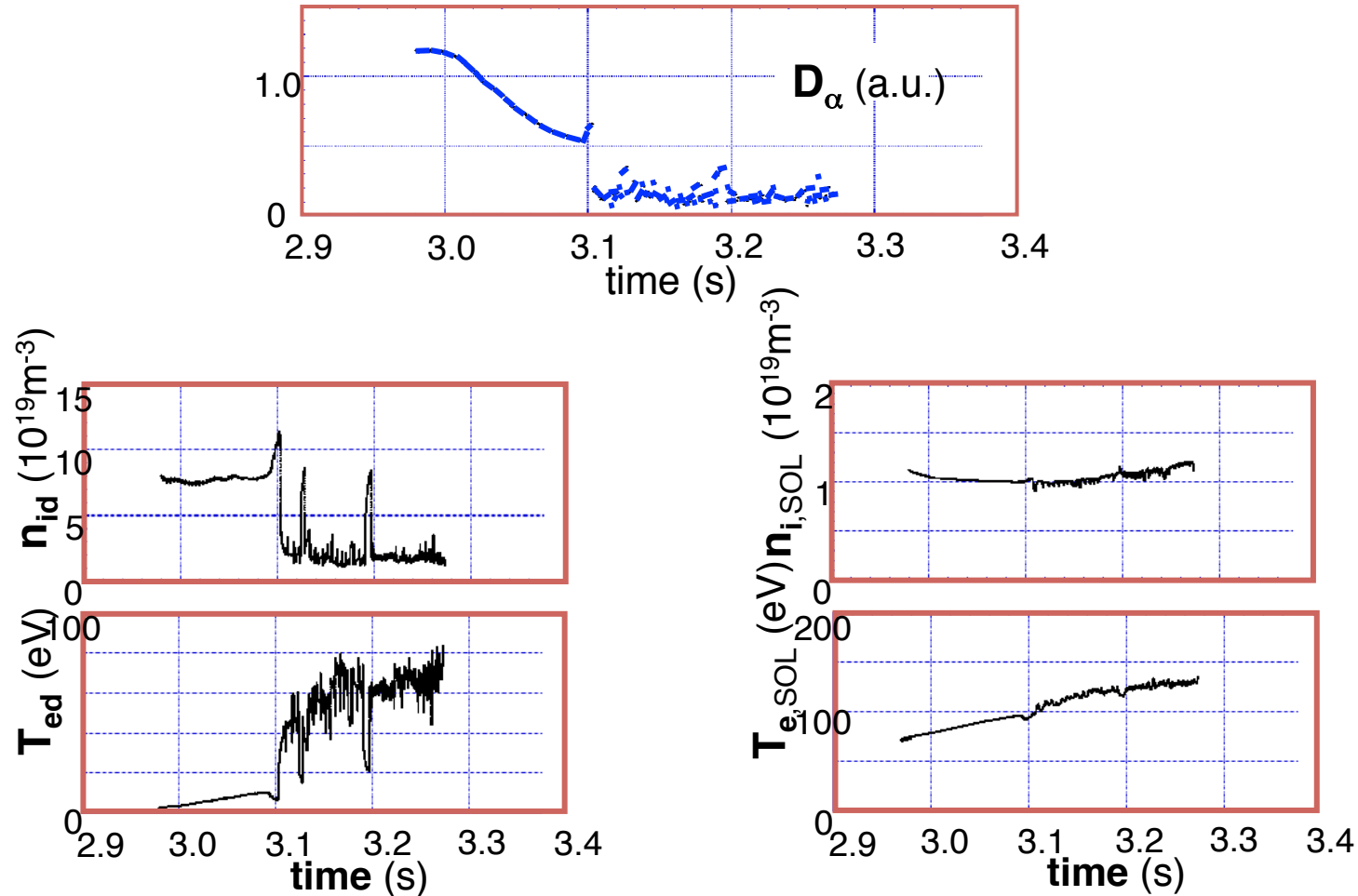
Evolution of electron density profile $n_e(r)$, electron temperature profile $T_e(r)$, and heat diffusivity profile $\chi(r)$. NB heating power is increased to 8 MW from the time $t = 3 \text{ s}$. An L/H transition occurs around $t = 3.1 \text{ s}$. χ is drastically dropped in the edge region and the pedestals are clearly formed on n_e and T_e profiles.

Turbulence Suppression by ExB Shearing Rate



After L/H transition, ExB shearing rate increment clearly overcomes the CDBM growth rate increment at the edge region.

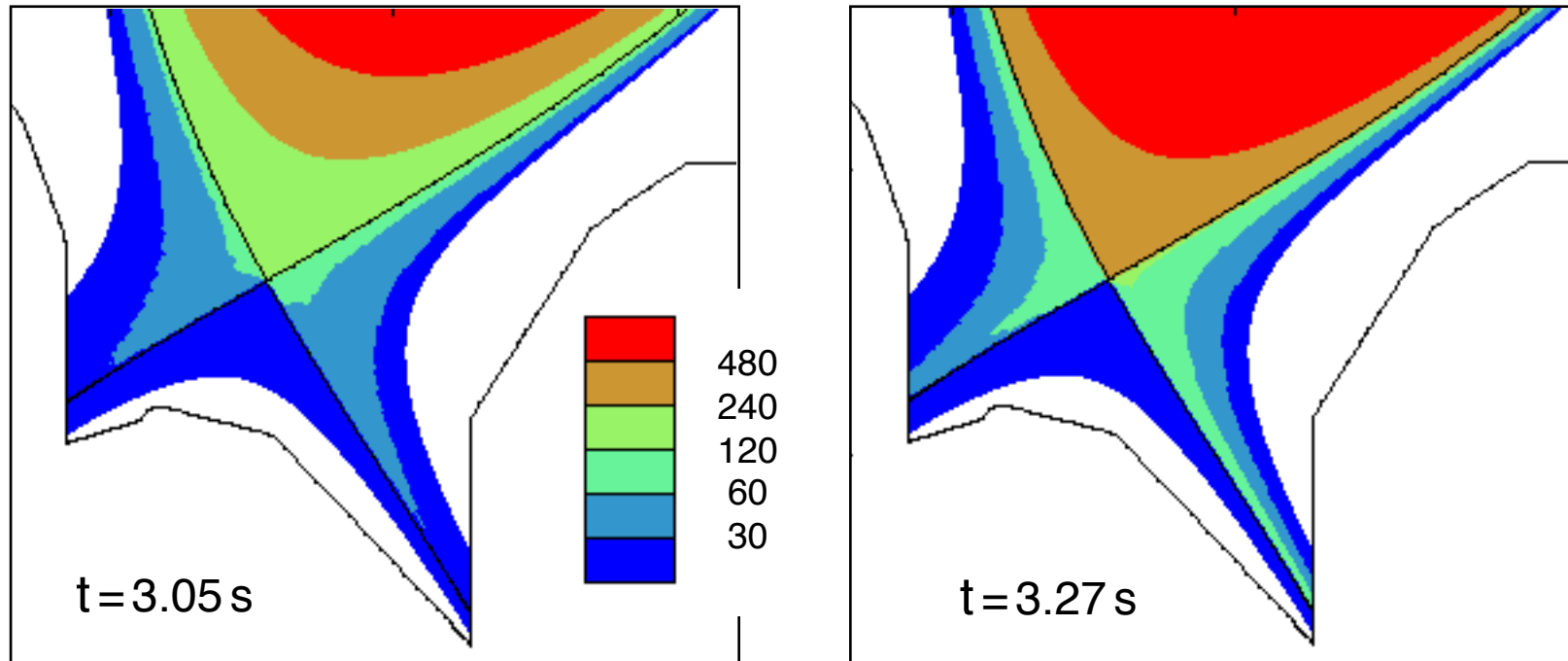
Time evolution of D_α and Profiles by SONIC



Time evolution of ion density and temperature (n_{id} , T_{ed}) at outer divertor strike point and ($n_{i,SOL}$, $T_{e,SOL}$) at outer mid-plane through the L/H transition.

Temporal fluctuation of SOL/divertor-plasma is observed in H-mode phase.

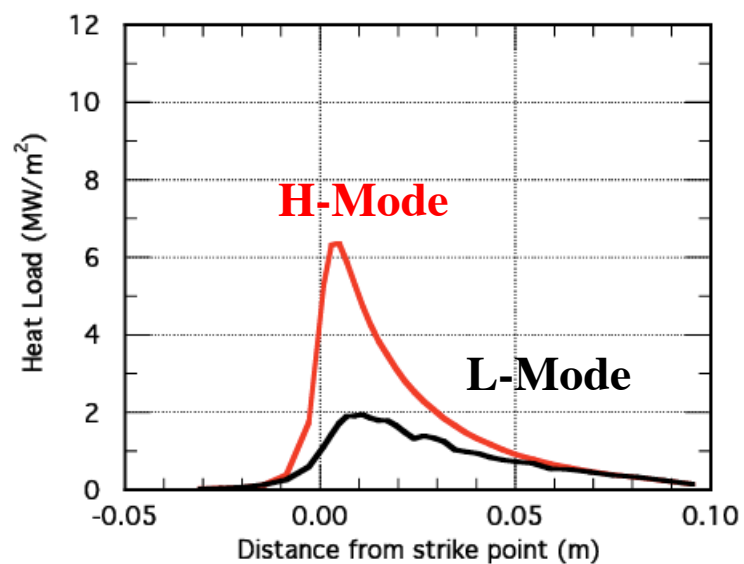
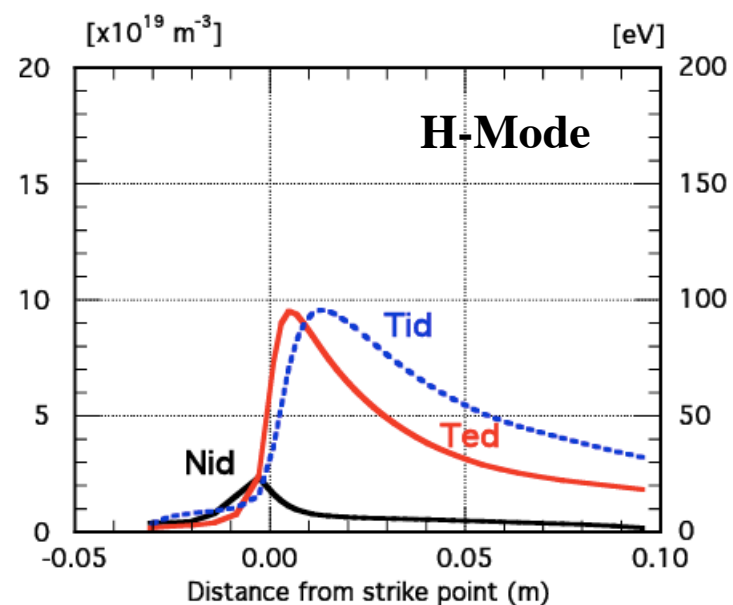
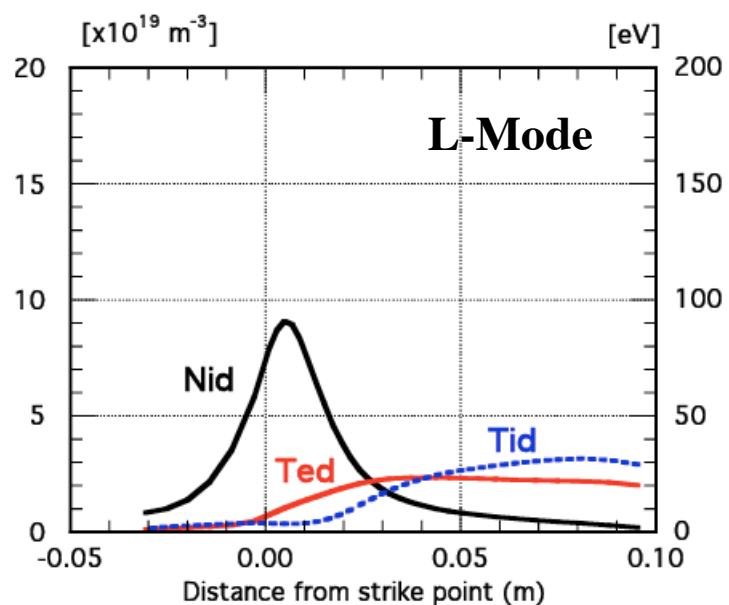
2D electron temperature before and after the L/H transition



After transition, electron temperature increases near divertor plate.

T_{ed} increases from $\sim 10 \text{ eV}$ to $\sim 50 \text{ eV}$.

Heat Load on Outer Divertor Plate



Summary

Self-consistent integrated modelling of core and SOL/divertor transport (TOPICS-IB & SONIC) is developed by MPMD parallel computing system.

The dynamic simulation for the L/H transition in JT-60SA is carried out by integrated code with tuned CDBM transport model including the $E \times B$ shearing effect.

Impacts of SOL/divertor transport on the L/H transition are studied. It is found that after the transition, the electron density suddenly drops and the electron temperature increases near the divertor plate. The temporal fluctuation of the SOL plasma is observed in the H-mode phase.

Examination of the numerical accuracy and analyses on the physical mechanisms are left for future work.